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(21) International Application Number: PCT/US92/03668 (22) International Filing Date: 4 May 1992 (04.05.92) (30) Priority data: 695,522                      3 May 1991 (03.05.91)                      US (60) Parent Application or Grant (63) Related by Continuation US    695,522 (CIP) Filed on                                      3 May 1991 (03.05.91) (71)(72) Applicant and Inventor: BURNHAM, Warren, R. [US/ US]; Drawer 312, Glens Falls, NY 12801 (US).		(74) Agent: KANANEN, Ronald, P.; Marks & Murase, 2001 L Street, N.W., Suite 750, Washington, DC 20036 (US). (81) Designated States: AT (European patent), BE (European patent), CA, CH (European patent), DE (European patent), DK (European patent), ES (European patent), FR (European patent), GB (European patent), GR (European patent), IT (European patent), JP, LU (European patent), MC (European patent), NL (European patent), SE (European patent), US. Published <i>With international search report.          Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>	
(54) Title: CATHETER WITH IRREGULAR INNER AND/OR OUTER SURFACES			
(57) Abstract			
A catheter is provided. The catheter has an irregular outer diameter (47, 48) and/or an irregular inner diameter caused by embedment of a reinforcing member (38), thereby reducing sliding friction compared to conventional smooth-wall catheters.			

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CATHETER WITH IRREGULAR INNER AND/OR OUTER SURFACES

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Background of the Invention

5           This invention relates to a method of making tubular products, especially catheters. More particularly, this invention relates to a method for making a reinforced catheter having an irregular lumen surface to reduce friction when used as a guiding  
10 catheter for the passage of another catheter through the lumen or the rotation of another catheter within the lumen. Still more particularly, this invention relates to a method of making a catheter wherein either or both elongated axial surfaces of a catheter are modified to  
15 decrease mechanical friction due to fluid coupling by causing the surfaces to have a non-linear or non-smooth character, thus to limit contact area with any adjacent structure to relatively small areas or line or points rather than the entire geometric surface or relatively  
20 large surfaces.

          As explained in U.S. Patent NO. 4,764,324, the art of manufacturing tubes, pipes or cannulae by extruding a plastic material to produce significant quantities of tubing is fairly well developed. In many  
25 instances, it is desirable to use reinforcement in the tubes or pipes to increase the pressure, tensioning, or torque-carrying capacities of those tubes or pipes. Ordinary plastic garden hose reinforced with filament is a common example of such a product made according to  
30 prior art techniques, as is a catheter for applications in the medical field.

          Catheters of the type contemplated are relatively thin and flexible tubes which include inner and outer plastic layers with a wire sheathing embedded  
35 between the layers wherein the wire sheathing is either braided or cross-wound to obtain maximum torsional rigidity and a satisfactory longitudinal flexibility. A convention prior art process for making a reinforced extruded catheter is a three-step process. In the first  
40 step, a mandrel having an outside diameter about equal to

the desired inside diameter of the finished catheter is passed through suitable extrusion tooling to cause a tubular jacket or sheath of the catheter material to form around the mandrel. In this step, the outside diameter of the first extrusion layer on the mandrel is smaller than the desired finished outside diameter of the finished catheter. Next, the inner core tube formed in the first step as described above is processed by suitable machinery to cause a pattern of reinforcing materials, such as wires, fibers, or monofilaments, for example, to be laid along and/or around or partially into and in contact with the surface of the core tube. Next, the composite intermediate structure of the inner core tube and the reinforcing layer thus applied is again passed through suitable extrusion tooling equipment to deposit a second layer of catheter material around and bonded to the composite thereby encapsulating the now reinforced inner core tube forming essentially a single structure. The outside diameter of the second layer of extrusion is approximately equal to the desired finished outside diameter of the catheter. Subsequently, finishing and polishing operations can be performed and a composite thus constructed cut to its desired length. The mandrel, if any, is then extracted by lengthwise pulling, leaving the hollow catheter tubing with reinforced walls. That process produces a catheter with smooth, uninterrupted inner and outer circumferential surfaces.

U.S. Patent No. 4,764,324 to the applicant herein constitutes a significant improvement on that three-step process by recognizing that heating the polymer substrate, or the reinforcing material and a polymer substrate beneath it, during a process of manufacturing a catheter, while simultaneously applying axial tension to the reinforcement, will cause the reinforcement material to deform or penetrate the original surface of the catheter body polymer and thus penetrate into such a surface. The distance to which the reinforcement material sinks into the underlying polymer

is highly controllable and repeatable depending on the conditions of the relative temperatures of the catheter body and the reinforcement material, as well as on the tension exerted on the reinforcing material, and the physical characteristics of the polymer from which the catheter is made. Thus, by controlling these parameters, the radial position of the reinforcement in the wall of the catheter can be simply but accurately followed. In the '324 patent, it had been noted that the polymer thus softened and deformed or penetrated but remaining outside of the new smaller diameter of the reinforcement structure produces a somewhat peaked or waffled contour in those locations where the polymer has exuded between the strands or filaments of the reinforcement and extends radially outwardly beyond the reinforcement to an extent where it can be worked to form the outer wall of the catheter body. However, the art suggested that smooth-walled catheters were desirable and users demanded such devices.

Accordingly, catheters made by either of the two processes noted above produced a catheter with a smooth inner diameter or bore well, or lumen, as well as a smooth, outer diameter wall to form a smooth surface composite construction of polymer containing the imbedded reinforcement between the now smooth inner and outer surfaces.

In fact, for most reinforced medical tubing structures, placement of the reinforcement strand is desired at or near the mid-wall point of the structure. In the '324 patent, the depth of radial placement of the reinforcement strand is chiefly controlled by the degree of heat softening of the substrate at the time the reinforcement impinges the surface under essentially constant application tension.

Among medical tube structures are those that are used as mechanical guides or sheaths. One such tube is the guide for balloon catheters in the practice of angioplasty. In this use, since a balloon-carrying catheter is to slide through the previously-placed

guiding catheter, it is desired to reduce internal friction between the guide tube and the balloon catheter to a minimum.

5           A smooth-walled guiding catheter, even one with a lining of a low friction material, such as a Teflon\brand material, can exhibit a considerable drag friction due to fluid coupling where a thin film of fluid "locks" the surface of the balloon to the catheter  
10 wall. An example of this phenomenon when air is the fluid can be found when meshing precision gauge blocks in a machine shop which, if pushed together tightly, will stick together even though there are no forces such as magnetism present. This occurs because the joint line  
15 between the blocks is so small that it does not readily allow air to enter the blocks to cause them to separate. Similarly, in the case of smooth-walled catheters and balloons, rubbing against the smooth guide tube wall displaces all but essentially a monolayer of the fluid  
20 present over a relatively large contact area,  $A = d l$  where  $d$  is the diameter of the lumen or I.D. of the tube; and  $l$  is the length of contact, allowing forces of molecular friction to create an unacceptably high drag friction.

25           Accordingly, it is a problem in the art, even in the use of standard smooth-bore catheters, and even when stiffness and torque properties are excellent and friction is low when dry, that high levels of fluid friction are experienced as soon as blood or injectate  
30 are present to make the fluid friction with the tube unacceptable.

          Accordingly, it is an overall problem addressed by this invention to develop a catheter and guide-tube pair which exhibit a marked reduction in axial and  
35 rotational drag forces during manipulation due to virtually complete elimination of viscous coupling between the adjacent surfaces.

          Accordingly, it is an object of this invention to provide a catheter having an inner bore or lumen with

an irregular surface to reduce contact friction when in use.

It is another overall object of this invention to provide a method and apparatus wherein either or both  
5 surfaces of a tubular object or the outer surface of a solid object are modified in such a way as to decrease mechanical friction due to fluid coupling by causing the surfaces to have a non-linear or non-smooth character, thus limiting contact area within the adjacent structure  
10 to small areas of points or lines rather than the entire geometric surface.

It is another overall object of this invention to provide a method and apparatus for producing a catheter with modified and controlled surface geometry by  
15 processes of embossing patterns on the outside surface and molding patterns into tubular inner surfaces.

It is still another object of this invention to provide a tubular catheter having a modified lumen surface wherein a reinforcing braid is submerged in a  
20 layer at the time of pattern of generation by use of a correctly sized die heated to a point where it heats and pushes the reinforcement (or pattern) into a substrate to cause waffle-like distortion of an outer wall surface of the structure.

25 These and other objectives of the invention will become apparent from the drawings and the detailed description of the invention which follows.

#### Summary of the Invention

30 Directed to achieving the forgoing objects and overcoming the problems of the prior art, this invention relates to a tubular object, such as a reinforced catheter, wherein the surface of the interior bore or lumen is irregular. In particular, the irregularity in  
35 the interior bore or lumen surface of the catheter is caused by placement of a reinforcement strand applied according to the teachings of the Applicant's prior U.S. Patent No. 4,764,324 to a location proximate but not through the interior wall, causing irregularity in the

lumen wall. Accordingly, the inner surface geometry is modified by displacement of the tube wall into the mandrel, thus exhibiting on the I.D. wall radially-raised ridges of maximum height directly under a reinforcement strand. Since the reinforcement strands are almost always in the form of a helical wrap along the axis of the tube, during the manufacturing process, the raised ridges take the form of helices along the tubing with the same hand as the innermost strands as applied.

10           The interior lumen or bore of the tubular catheter thus has its normally smooth surface interrupted by a pattern which eliminates the problem of fluid coupling because contact between stationary and moving members is along the line or innermost surface of the raised ridges, rather than across and along the entire lumen surface.

          In another aspect, the applicant's invention relates to surface modification of the external surface of a solid or tubular object, such as the catheter, to reduce friction as noted above, especially when the catheter is moved through or rotated within a guiding catheter. The exterior surface of the object to which a reinforcement was applied, according to the teachings of the '324 patent, exhibit an elongated diamond-like or waffle-like pattern generated on the outer surface by the entry by right and left hand reinforcement helices. Rather than completely smooth over the "diamonds" or "waffles", a smoothing step is eliminated, or an oversized die is used to perform an intentionally incomplete smoothing step, leaving a pattern of smooth-tipped waffles or diamonds on the outside tube surface. While normally such a rough outer tube surface would be discarded as unsuitable for vascular contact, it was found that such a surface has significant advantages when the tube was used to slide concentrically down the lumen of an outer tube acting as a guide tube or to be rotated within a guide tube.

          According to another aspect of the invention, a method of making such a tube is provided according to



the steps of the '324 patent comprising a continuous method for making a finished reinforced catheter made from a polymeric material exhibiting a range of apparent viscosity proportional to temperature and having an inner  
5 diameter and an outer diameter with reinforcement completely embedded within the wall of the tube between the inner diameter and the outer diameter.

The method comprises the steps of providing as an interim structure an extruded, mandrelized polymeric  
10 catheter body having an outer diameter about equal to the outer diameter of the finished catheter; providing the mandrelized catheter body in a condition heated to a state sufficient to prevent a reinforcing member under tension to be submerged completely beneath an outer  
15 surface of the heated tubular structure to a location adjacent to the inner diameter; and applying the reinforcing member at the outer surface of the heated interim mandrelized catheter body under sufficient tension to cause the reinforcing member to travel  
20 inwardly through the polymeric outer surface to a predetermined extent to deform the outer surface relative to the reinforcing member by a volume about equal to the volume of the reinforcing material added to the tubular structure. In one aspect of the invention, the process  
25 contemplates not smoothing the irregular surface so formed or smoothing the outer surface of the reinforcing catheter with an oversized die to permit the outer surface to remain irregular.

In another aspect of the invention, the  
30 reinforcing material added to the tubular structure is located accurately in the wall of the body adjacent to or near or sufficiently near the inner diameter to cause a distortion thereof, thus to cause inner surface irregularity or irregular contours determined by the  
35 reinforcement. Thus, the combination of temperature and material of the catheter and tension on the reinforcing member controlling the location of the reinforcing member to the position noted will produce a catheter having the thus-modified surface structure(s).

These and other features of the invention will become apparent from the detailed description of the invention which follows, taken with the accompanying drawings.

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### Brief Description of the Drawings

In the drawings:

Fig. 1 is a block diagram of a prior art process for manufacturing an intermittently reinforced catheter with an unitary reinforced tip;

Fig. 2 is a pictorial diagram partially in perspective, showing the catheter structure as it progresses through the manufacturing process diagrammed in FIG. 1;

Fig. 3, including Figs. 3A-3E, are cross section of the composite catheter structure at various steps in the prior art process depicted in FIGS. 1 and 2;

Fig. 4 is a block diagram of an improved prior art the process suitable for making the catheter according to the invention;

Fig. 5 is a pictorial diagram, partially in perspective, showing the structure of the invention at various stages in the manufacturing process of Fig. 4;

Fig. 6, including Figs. 6A-6F, illustrates cross sections of the composite structure at various stages in the process shown in Figs. 4 and 5 according to the invention;

Fig. 7 is a series of cross-sectional views of distortions of the interior wall and mandrel according to the invention, wherein Fig. 7A shows in diagrammatic fashion a cross-sectional view of a mandrelized tube showing distortions of the interior wall of the tube and the exterior wall of the mandrel according to the process; Fig. 7B shows an enlarged view of the same; and Fig. 7C shows an axial view of the same;

Fig. 8 shows in Fig. 8A a cross-sectional view of the tube after removal of the mandrel; and Fig. 8B

shows an elongated axial section thereof showing the interior surface of the tube;

Fig. 9A shows the external surface made according to the processes of Figs. 4 and 5 in a view similar to Figs. 6C and 6D but unsized or sized by an oversized die; and

Fig. 9B shows the exterior surface of the tube made according to the prior art process of Figs. 1 and 2 without the second pass.

10

#### Detailed Description of the Preferred Embodiments

Figs. 1-3 describe in greater detail a prior art process for manufacturing a reinforced tube, for example, a catheter, as designated generally by the reference numeral 15. As shown in Figs. 1-3 a mandrel 17, from a mandrel source 16, comprises an elongated tubular or solid form 17 having a generally circular cross section (Fig. 3A) is passed through an extruder 19 to provide a sheath 20 of plastic material about the mandrel 17. The mandrel 17 has an outside diameter equal to the desired inside diameter of the finished catheter 15. The innermost layer of the catheter wall is formed from the sheath 20 to form a base tube for the finished catheter and has an inside diameter equal to the outside diameter of the mandrel 17. The plastic sheath 20 about the mandrel 17 during the first extrusion step has an outside diameter which is smaller than the desired finished outside diameter of the finished catheter.

The inner base tube 21 formed as described above is processed by suitable machinery 22, known to the art, to cause a pattern of reinforcing material 23 to be laid along and/or around or partially into or in contact with the outer surface of the core tube 21. By way of example, the reinforcing material may include wires, fibers or monofilaments. Where desired, the composite catheter structure with the reinforcing material 23 may be processed to intermittently excise a portion of the reinforcement, as shown generally by step 25. In performing this step, the reinforcement material thus

formed is physically removed along spaced portions of the core tube 21, as shown at portion 26 of Fig. 2. Thereafter, the core tube 21 with reinforcement spacedly excised is passed again through an extruder 27 to form a  
5 second layer 28 of extruded wall material as a sheath and bonded to the composite to produce a composite structure having an outer diameter of the catheter. In performing this step, therefore, the reinforcing layer 23 (whether or not partially excised) is thus embedded in the wall of  
10 the final composite catheter structure 28, which wall comprises two radially located sequentially applied extrusion layers bonded together to form a structurally single tube wall. Finally, in the step designated generally by the reference numeral 30, the composite thus  
15 constructed may have its wall smoothed to a tolerance of about  $\pm 0.0005$  inches; is cut to its desired length; and the mandrel 17, is extracted by lengthwise pulling leaving the hollow catheter tubing with intermittent or continuous reinforced walls.

20 A process for making the tube, such as a reinforced catheter, according to the invention is best seen in its preferred embodiment in Figs. 4-6. In Fig. 4, the prior art Burnham process is designated generally by the reference numeral 32. As a starting material for  
25 the process 32, a mandrel 34 from a mandrel source 33 is passed through an extruder 35 to deposit a sheath 36 about the mandrel 34 in a manner somewhat similar to the first extrusion step of Figs. 1 to 3. However, the outside diameter of the extrusion here is approximately  
30 equal to the full outside diameter of the finished catheter and is the only extrusion step performed.

Reinforced material 38 is applied to the mandrel/tubing composite structure 39 in a manner similar to that described in connection with Fig. 1. However, it  
35 has been found that the application of heat by a suitable heat source 40 to the mandrelized wall tubing acting as a starting material and/or to the reinforcing material 38, while simultaneously tensioning the reinforcing material by a tensioning device 42 will cause the

reinforcing material when applied to the original surface of the catheter body to sink into such surface and to penetrate or deform it. The heat thus applied to a thermoplastic material forming the catheter body causes  
5 the thermoplastic polymer to soften to an extent sufficient to permit such penetration or deformation.

It has been found that the distance into which the reinforcement material penetrates beneath the surface of the catheter body and thus sinks into the underlying  
10 polymer is highly controllable and repeatable. That distance is a function of the relative temperatures of the catheter body and/or the reinforcement material, as well as the simultaneous tension exerted on the reinforcing material by the tensioning device, and the  
15 material of the body. Thus, by way of example, if the temperatures applied to the catheter body and the reinforcing material are controlled within toleranced limits, for a given catheter body made from a known polymer exhibiting known viscosity as a function of  
20 temperature, the depth of penetration of the reinforcing material can be determined for a given process rate and time of application virtually solely by the degree of tensioning applied by the tensioning device.

An alternative practice of the process,  
25 assuming that the tensioning is fixed within toleranced limits, the degree of heating of the catheter body and/or the reinforcement material, will similarly control the dept of penetration at a constant process speed. In its simplest form, controlling the temperature of the heat  
30 source 40 will control the degree of heating of the catheter body composite at that stage in the process. Since the process is practiced on a continuous basis, the heating temperature may also be controlled by the speed of the process, by way of example, by passing the  
35 mandrelized catheter body through a heat source 40 providing a source of heat within toleranced limits. One way of applying heat to the catheter body 36 is by passing the catheter body 36 through an oven, or through a fluid heat transfer medium for a time sufficient to

permit the catheter body 36, or at least the radially-outwardly extending portion of the catheter body 36, to soften to an extent which permits it to receive the reinforcing material 38 therewithin. Another way is by heating the reinforcing material which in turn heats the polymer.

As explained in the '324 patent, such a process had significant advantages in controlling the placement of the reinforcement material 38 in the wall of the catheter body 36 and thus is particularly suited for applications in which it is necessary to structure a catheter such that the reinforcing material 38 is located near the outer wall of the catheter, near the inner wall of the catheter, or at a precisely-controlled selected point in between. When it is remembered that catheter bodies are extremely small structures and catheter walls are extremely thin, such a process has significant advantages in assuring that the reinforced materials are embedded within the catheter wall throughout the length of the catheter while at the same time omitting the second extrusion step as previously discussed in connection with Fig. 1.

Fig. 5 and Fig. 6A-6F further illustrate the features of this aspect of the invention. Following the submersion of the reinforcing material 38 into the catheter body 36 mad from a thermoplastic polymer, the polymer thus softened and penetrated, but remaining outside the new smaller diameter of the reinforcement structure, produces a peaked or waffled contour, designated generally by the reference numeral 46 (Fig. 6C) in those locations where the polymer has exuded between the penetrating strands of the reinforcing material 38. The volume of polymer material from the reinforcement structure which is displaced is about equal to the volume of the reinforcing material 38 submerged in the catheter body. Thus, in Fig. 6C, the outside diameter of the composite catheter prior to application of the reinforcing material is designated by a dotted line by the reference numeral 47 to illustrate that in

general the peaked areas 46 extend beyond the former outside diameter of the catheter body, while the valley areas formed near the wire (designated generally by the reference numeral 48) generally inwardly peak at the location of the reinforcing material 38 at a radially outwardly extending distance less than that of the former outside diameter 47 of the catheter body. Such a formed structure is advantageous in that in subsequent normal processing, the protruding portions 46 may be smoothed over in a sizing and/or smoothing step 44 to form a smooth catheter wall completely enveloping and embedding the reinforcement material 38 as seen in Figs. 6E and 6F. More significantly, such a step avoids the application of a second extrusion.

According to one aspect of this invention, however, a catheter having an outside contour as shown in Figs. 6C and 6D may be passed through an oversized die, or left merely so solidify or cure with the contour there shown. This leaves the irregular surface 46, 47 of the catheter 38 as the outer finished catheter surface. If the catheter does not pass through a die, (eliminating step 44) the effective contact area of the irregularity, i.e., "diamond" or "waffle", is determined by one or more lines at the largest effective O.D. Such line contact then determines the frictional engagement while fluid coupled to the guiding catheter.

On the other hand, if the surface of Figs. 6C and 6D passes through an oversized die, a somewhat flattened outer surface is formed, as seen in Fig. 9B, where each protrusion has an upper area  $A_i$  so that the entire surface area at the effective O.D. of the tubular catheter is  $A = \sum A_i$  for a given length, and  $A = \frac{\pi d^2 L}{4}$ , where  $d$  is the outer diameter and  $L$  is the length.

In another preferred aspect of the process according to the invention, the composite reinforced catheter body construction produced according to the invention may have the reinforcement material 38

intermittently applied, as in the prior art, or by continuously applying the reinforcement material and then excising portions thereof, or by periodically stopping the application of the reinforcement material, or  
5 continuously applying the reinforcement but in such a way as to cause the reinforcement material to lie along the outer surface of the composite structure as a series of straight line strands, as shown in Figs. 8-10 of the '324 patent (herein incorporated by reference) as is there  
10 explained in greater detail. Such a straight line pattern is not submerged into the catheter wall body and thus is easily removed from the surface of the composite structure.

The process of the invention may be performed  
15 continuously utilizing conventional machinery. Thermoplastic polymer mandrels, extruders, and machines for applying reinforcing material, such as modified braiders, are known to the art. For example, braiding machines are available from either New England Butt  
20 Company or Wardwell Company, by way of example.

As specific examples of the type of thermoplastic plastic materials which may be used, such materials include polyethylene, polyurethane, certain rubbers, latexes and vinyls, conventionally available  
25 from such companies as DuPont. As a specific example of a preferred reinforcement material, one may use polyaramid, which is commercially available under the trademark "KEVLAR", but other materials such as carbon, boron fiber, glass, ceramic, non-metallic wires, metallic  
30 wires, and natural fibers such as cotton, as well as monofilaments such as nylon and polyester, may also be used. Where it is desired to utilize the reinforcement material as a conductor for signals, an electrically conductive wire may be used as all or any part of the  
35 reinforcement material.

The embodiment of Fig. 4 has been described with respect to the thermoplastic polymers forming the catheter body, using heat as the medium for controlling the plasticity of the wall to permit penetration of or



deformation by the reinforcing material to form the waffled contour 46. In the alternative, as shown by the step bearing the reference numeral 49, other curable polymers may also be used. Where, for example, the polymer may be hardened by curing the cross-linking under the application of ultra-violet light, or by ionizing radiation, a curing step particular to the curable resin may be used. Such curable polymers may possess a sufficiently semi-rigid body characteristic prior to curing to permit penetration into, or deformation of, the surface by the application of the reinforcement material, as previously described, or to form the waffled contour without the application of heat at the reinforcing application as described in connection with Fig. 4. In those instances, the step of applying simultaneous heat may be eliminated in favor of a curing step, which may be a heating step, after the application of the reinforcement material and/or its partial excising as described and during or after sizing as shown in step 44. These alternative times of application of the curing step subsequent to the application of the reinforcement material to the catheter body being formed are designated generally by the two arrows connecting the block 49 to the process of Fig. 4. However, depending on the characteristics of the material used, a curing or partial curing step may be carried out either earlier or later in the process while carrying out the essential features of the invention.

In still another preferred aspect of the invention, for the mandrelized embodiment of either Figs. 2 or 4 made according to the processes of Figs. 1 and 4 respectively, the reinforcing material can be caused to be positioned in the mandrelized tube as shown in Fig. 7, and in particular in Fig. 7A. Such an embodiment was discovered during experimental runs of steps in the '324 patent wherein it was learned that it is possible to insert the reinforcement "too deeply" within the wall, 36, to a location that is almost through the wall 36 into the lumen location, stopping just short of breaking

through the interior wall 70. Since the mandrel 34 used during the processing is itself polymeric in nature, the heat softening of the structure wall 36, 70 as described above also carries slightly into the mandrel 34 as shown  
5 in the arc of the circle 90 defined by a locus of points equidistant from the outer surface of the reinforcing member 38. The result thus is that although the reinforcement strand 38 can be kept from passing completely through the structural wall 70 into the  
10 mandrel 34, the displacement of catheter body material ahead of the strand, i.e., in the partial annulus 91, can be made to carry into the outer surface or the mandrel 34 with the result that when the mandrel 34 is removed, the displacement of the tube wall into the mandrel shows as  
15 a radially raised ridge 71 of maximum height 72 directly, radially from the reinforcement strand.

Moreover, as seen in Figs. 7A to 7C, since the reinforcement strands 38 are almost always in the form of a helical wrap along the axis of the tube, the raised  
20 ridges 71 take the form of helices down the tubing with the "hand" of the innermost strand of set of strands as applied.

While not completely understood, the raised ridges assume a contour which is defined by about a locus  
25 of points of material equidistant from and having about the same shape as the reinforced strand. Thus, as seen in Figs. 7A to 7C, the raised ridges 71 are defined by at least an arc of a circle and at most by a semicircle.

The interior wall of the catheter bore has a  
30 plurality such ridges 71, as seen in Figs. 8A and 8B after the mandrel 34 is removed. The area of the high points is essentially a line contact 72, but if desired, though definitely not preferred, the ridges 72 could be smoothed and thus flattened somewhat to define an area  
35 having a relationship like that discussed for the outer relationship.

The method of Fig. 1 may also be used according to the teachings of the '324 patent so long as the

exterior wall or interior wall exhibit the properties noted in this invention.

Fig. 8 illustrates in greater detail the features of the invention relating to the tube after removing the interior mandrel. Thus, the interior wall exhibits a "rifling" characteristic. As used, "rifling" is descriptive of the single-handed helical protrusion of the inner wall of a tubular structure due to the influence of the innermost of the two helices applied according to the '324 process in such a way as to almost breach the inner wall without doing so.

Figs. 9A and 9B show the exterior surface of the tube whether made according to the process of Figs. 4-6 or according to the process of Figs. 1 and 2. For example, for a tube made according to the process of Figs. 4-6, thus producing a tube with a cross section and axial section shown in Figs. 6C and 6D, the tube is sized with a sizing and smoothing die which is oversized. Thus, rather than produce a surface such as shown in Figs. 6E and 6F, the surface is intentionally incompletely smoothed, leaving a pattern of smoothed-tip "waffles" or "diamonds" on the outside surface of the tube as shown in Fig. 9A. Such a rough surface tube would normally be discarded as unsuitable for vascular contact, but is advantageous in permitting the tube to slide concentrically down the lumen of an outer tube. Thus, the outer sheath of a tube so constructed exhibits the same low friction phenomena in the presence of fluid on the outside of the catheter as on the inside surface of the tube according to the invention. Accordingly, break up of fluid coupling occurs because of the waffled outer surface in a manner similar to the fluid coupling break up caused by the rifled interior surface as previously described. "Waffling" may be considered to be descriptive of the almost rectangular continuous pattern generated on the outer surface of a softened polymer structure by the passage through it of tensioned reinforcing strands. These strands are usually applied in the form of two, oppositely-handed helices of one or

more strands each. As the strands are simultaneously wrapped into the tubed structure, each strand plows up a lineal distortion of the surface leaving a slightly depressed groove behind it as it sinks in. As these  
5 opposite-handed grooves cross each other, they leave a cross hatched pattern herein described as a "waffle" as well as raised "pillows" of polymer resulting from partial volumetric placement by the strand cross sections.

10 Finally, the method and apparatus according to the invention may exhibit both characteristics. That is, a tube made according to the invention may have the rifled inner tube as shown in Figs. 8A and 8B, and the waffled outer surface as shown in Figs. 9A so that the  
15 tube may be made for use as either a guiding catheter for a smaller interior catheter, or as a guided catheter in a larger tube.

Thus, an improved reinforced tube or catheter, and a method of making such an improved tube or catheter  
20 with superior interior and/or exterior surface characteristics has been described.

As a representative example, a catheter according to the invention has been made according to the teachings of the '324 patent and this application with an  
25 O.D. of 0.104", and ID of 0.080", and a wall thickness of 0.012" having a wire reinforcement of 1 to 3 mils precisely embedded in the wall to produce the ID irregularity as described.

This invention will also provide a tubular  
30 catheter with a modified lumen and/or outside surface by modification of the prior art process of multiple layer extrusion. The lumen surface modification is accomplished at the time the reinforcing is being applied to the undersized "core" extrusion by use of a heated die  
35 located on the braiding machine slightly above the formation point of the braid.

This die is slightly smaller than the combined diameters of the first extrusion and the braid laying on its surface. The combination of the intentional

interference fit and the heat of the die causes the reinforcement to be forced into the polymer structure as a path of least resistance. The heat present is controlled in degree so that the polymer layer is not fused completely. The compression of the reinforcement due to the heated die causes the braid to sink in to a predetermined level, but since the polymer is un-melted, that portion under the reinforcement strands is forced radially inward more than the polymer not directly under the reinforcement strand, thus reflecting the pattern of the braid without the reinforcement actually penetrating through the polymer layer and into the lumen. Upon removal of the temporary support mandrel from the lumen, the image of the braid pattern shows as a "waffle" of the lumen surface, the irregularity of which exhibits the friction reducing properties claimed in this invention.

Patterning the outside surface is accomplished during extrusion of the outer jacket by intentionally extruding at a lineal rate too fast to allow the melt to reach volumetric pressure equilibrium around the radially projecting portion of the reinforcement. This results in an outwardly projecting image of the reinforcement pattern, thus accomplishing the desired result of friction modification by contact area reduction.

A stainless steel reinforced polymer tube may also be provided which exhibits variable bending stiffness, with the variations occurring over the length of the tube at controlled locations and to a controlled degree and for a controlled axial length. The embodiment produced the following:

**Embodiment specs:**

Polymer Tube -- .081" ID x .106 OD

Pebax 72D

Reinforcing -- 001" x .005" 304LV Stainless Flat

Wire

Variable Pattern Density -- 10 to 32 picks or crosses/lineal inch axial

The invention may be embodied in other specific forms without departing from its spirit or essential characteristics. The present embodiments are, therefore, to be considered in all respects as illustrative and not  
5 restrictive, the scope of the invention being indicated by the claims rather than by the foregoing description, and all changes which come within the meaning and range of the equivalents of the claims are therefore intended to be embraced therein.

What is Claimed Is

1           1.    A finished reinforced catheter made from  
2 a polymeric material and having a bore with an inner  
3 diameter and an outer diameter with a reinforcement  
4 member completely embedded within the wall of said  
5 catheter between said inner diameter and said outer  
6 diameter, said reinforcement material being embedded  
7 sufficiently close to said inner diameter as to provide  
8 at least a ridge interrupting the smoothness of said  
9 inner diameter and following the contour of the  
10 reinforcement material located adjacent thereto, said  
11 ridge defining a land having an effective I.D. less than  
12 an and actual I.D. of said interior diameter, so that  
13 when used as a guiding catheter, the effective friction  
14 force on an axially inserted or rotated concentric  
15 catheter is less than that exhibited by a smooth I.D.  
16 wall.

1           2.    The catheter as set forth in claim 1,  
2 wherein said ridge is shaped in cross section about as an  
3 arc of a circle for a circular reinforcement member.

1           3.    The catheter as set forth in claim 1,  
2 wherein said ridge is approximately semicircular for a  
3 circular reinforcement member.

1           4.    The catheter as set forth in claim 1,  
2 wherein the shape of said ridge is a raised band due to  
3 use of a flattened wire with one axis of a length greater  
4 than the other.

1           5.    The catheter as set forth in claim 1,  
2 further comprising a plurality of such ridges spaced  
3 about along the interior of the inner diameter bore of  
4 said catheter.

1           6.    A method of using the catheter of claim 1  
2 as a guiding catheter comprising the steps of providing

3 the catheter as defined in claim 1, and passing another  
4 catheter therethrough whereupon contact between the outer  
5 surface of said passing catheter and said guiding  
6 catheter is defined by said interior ridge, thus reducing  
7 fluid coupling therebetween.

1           7. The catheter as set forth in claim 1,  
2 further including wherein said outer diameter further  
3 includes an irregular surface, thus reducing the friction  
4 of said outer diameter when said catheter is guided  
5 through another tubular member.

1           8. The catheter as set forth in claim 1,  
2 further including wherein said outer diameter further  
3 includes an irregular surface, thus reducing the friction  
4 of said outer diameter when said catheter is guided  
5 through a ridged internal lumen wall.

1           9. A finished reinforced catheter made from  
2 a polymeric material and having a bore with an inner  
3 diameter and an outer diameter with reinforcement  
4 completely embedded within a wall of said catheter  
5 between said inner diameter and said outer diameter, said  
6 outer diameter exhibiting an irregular surface caused by  
7 embedding said reinforcement in said catheter made from  
8 a polymeric material exhibiting a range of apparent  
9 viscosity proportional to temperature, said outer surface  
10 of said catheter deforming relative to said reinforcing  
11 member by a volume about equal to said reinforcement  
12 material added to said tubular structure.

1           10. A continuous method of making a finished  
2 reinforced catheter made from a polymeric material  
3 exhibiting a range of apparent viscosity proportional to  
4 temperature and having an inner diameter and an outer  
5 diameter with reinforcement completely embedded within  
6 the wall of said catheter between said inner diameter and  
7 said outer diameter with a single extrusion step  
8 comprising the steps of:



9 providing as an interim structure an extruded,  
10 mandrelized polymeric catheter body having an outer  
11 diameter about equal to the outer diameter of the  
12 finished catheter;

13 providing said mandrelized catheter body in a  
14 condition heated to a state sufficient to permit a  
15 reinforcing member under tension to be submerged  
16 completely beneath an outer surface of the heated tubular  
17 structure;

18 applying said reinforcing member at the outer  
19 surface of the said heated interim mandrelized catheter  
20 body under sufficient tension to cause said reinforcing  
21 member to travel inwardly through said polymeric outer  
22 surface to a predetermined extent to deform said outer  
23 surface relative to the reinforcing member by a volume  
24 about proportional to the volume of said reinforcing  
25 material added to said tubular structure and to locate  
26 the reinforcing member accurately in the wall of said  
27 body thus defining wall portions which lie radially  
28 outwardly and inwardly of the former outer diameter of  
29 the catheter body, a combination of the temperature and  
30 said polymeric material of said interim catheter and  
31 tension on said reinforcing member controlling said  
32 predetermined extent, the location of said reinforcing  
33 member within the finished product being defined by the  
34 location of said reinforcing member when applied to said  
35 interim catheter body, said deformed outer wall being the  
36 outer wall of said catheter.

1 11. The method of claim 10 wherein said  
2 catheter is made from a thermoplastic resin, and the step  
3 of applying includes the step of heating said mandrelized  
4 catheter body and/or said reinforcement to a degree which  
5 sufficiently softens the catheter body to permit  
6 deformation or penetration when said reinforcing member  
7 is applied thereto.

1 12. The method as set forth in claim 11  
2 wherein the step of heating is accomplished only by

3 heating said reinforcing member when applied to said  
4 catheter body.

1           13. The method as set forth in claim 12  
2 wherein the step of applying further includes the step of  
3 tensioning the reinforcing member while being applied to  
4 said catheter body to cause said reinforcement member to  
5 deform the outer surface of said catheter body.

1           14. The method as set forth in claim 11  
2 wherein the step of applying further includes the step of  
3 tensioning the reinforcing member while being applied to  
4 said catheter body to cause said reinforcement member to  
5 deform the outer surface of said catheter body.

1           15. The method as set forth in claim 10  
2 wherein the step of applying includes the step of  
3 tensioning the reinforcement member while being applied  
4 to said catheter body while controlling the tension on  
5 said reinforcing member while being applied thereto thus  
6 to control the depth of penetration of the reinforcement  
7 member beyond the outer surface of said catheter body  
8 toward the axis thereof, thereby to control the location  
9 of said reinforcement member in said finished catheter at  
10 a location which deforms the inner wall of said catheter.

1           16. The method as set forth in claim 10  
2 wherein said catheter body is made from a thermoplastic  
3 material, and wherein the step of applying includes the  
4 step of heating said thermoplastic catheter body  
5 sufficient to permit the reinforcing member to cause the  
6 outer surface of said catheter body to become irregular  
7 when applied thereto.

1           17. The method as set forth in claim 16  
2 wherein the step of heating includes the step of heating  
3 both the thermoplastic catheter body and the  
4 reinforcement member while being applied thereto.

1           18. The method as set forth in claim 10  
2 wherein said reinforcing member is a braid comprising a  
3 plurality of reinforcing members applied to said catheter  
4 body in a spaced array.

1           19. The method as set forth in claim 10  
2 further including a step of sizing said irregular  
3 deformed outer wall with an oversized die.

1           20. A continuous method of making a finished  
2 reinforced catheter from a thermoplastic material having  
3 an inner diameter and an outer diameter with a single  
4 extrusion step and without application of pressure from  
5 an external source to said inner diameter comprising the  
6 steps, of:

7           continuously extruding a mandrelized catheter  
8 body as an interim structure having an outer diameter  
9 about equal to the outer diameter of said finished  
10 reinforced catheter;

11           heating said mandrelized catheter body to a  
12 temperature to causes aid thermoplastic material to  
13 exhibit a predetermined degree of viscosity;

14           continuously applying a tensioned length of a  
15 reinforcing member to an outer surface of said heated  
16 interim catheter body by a guide rotating in a plane  
17 approximately normal to movement of the catheter body to  
18 define a helix angle determined by the ratio of the  
19 length through which the tube advances for each complete  
20 rotation of the guide;

21           the step of applying being carried out while  
22 said catheter body is sufficiently viscous to permit  
23 deformation at a surface contour of said catheter body by  
24 an amount at least equal to the volume of said  
25 reinforcing member through a wall of said catheter body  
26 to locate said reinforcing member entirely therein at a  
27 location determined by said viscosity and tension on said  
28 reinforcing member while the length of reinforcing member  
29 is applied thereto; and

30           said location interrupting said inner diameter  
31 to cause said inner diameter to become irregular, thus to  
32 define at least a land having an I.D. less than the I.D.  
33 of said inner diameter.

1           21. The method as set forth in claim 19  
2 including the step of ceasing the rotation of said guide  
3 to cause said reinforcing member to lie along the surface  
4 of said catheter body for a length determined by the time  
5 in which rotation in which said guide has ceased relative  
6 to the movement of the tube in its axial direction,  
7 thereby to facilitate excision of said reinforcing  
8 material along said length to form a unitary catheter.

1           22. A method as set forth in claim 19 further  
2 including the step of applying at least a second length  
3 of reinforcing material to said catheter body, said first  
4 length being applied at a first helix angle which is  
5 large relative to the axis of the catheter body, the  
6 second length being applied at a small angle relatively  
7 to said axis, the application of a multiple set of helices  
8 to the catheter body being controlled to produce precise  
9 torque and stiffness characteristics for the finished  
10 catheter.

1           23. A method according to claim 19, wherein  
2 said reinforcing member is an electrically conductive  
3 material adapted as a conductor for electrical signals.

1           24. A method according to claim 19, wherein  
2 said reinforcing member is an electrically conductive  
3 material adapted as a partial number of the plural  
4 strands.

1           25. The method as set forth in claim 22  
2 further including a smoothing step to smooth the other  
3 surface of said elongated product after said reinforcing  
4 member has passed therethrough, so that the final surface  
5 of the finished product can be developed with a smoothing

6 step while eliminating a requirement for a second  
7 extrusion step to produce said final surface of said  
8 finished product.

1           26. A method according to claim 20, wherein  
2 all or a part of said reinforcing member is an  
3 electrically conductive material adapted as a conductor  
4 for electrical signals.

1           27. The method of claim 20 wherein said  
2 catheter is made from a thermoplastic resin, and the step  
3 of applying includes the step of heating said mandrelized  
4 catheter body to permit deformation or penetration when  
5 said reinforcing member is applied thereto.

1           28. The method as set forth in claim 27  
2 wherein the step of heating alternatively includes the  
3 step of heating said reinforcing member while being  
4 applied to said catheter body to cause said reinforcement  
5 member to deform the outer surface of said catheter body  
6 to form said irregular outer surface.

1           29. The method as set forth in claim 28  
2 wherein the step of applying further includes the step of  
3 tensioning the reinforcing member while being applied to  
4 said catheter body to cause said reinforcement member to  
5 deform the outer surface of said catheter body to form  
6 said irregular outer surface.

1           30. The method as set forth in claim 27  
2 wherein the step of applying further includes the step of  
3 tensioning the reinforcing member while being applied to  
4 said catheter body to cause said reinforcement member to  
5 deform the outer surface of said catheter body to form  
6 said irregular outer surface.

1           31. The method as set forth in claim 20  
2 wherein the step of applying includes the step of  
3 tensioning the reinforcing member while being applied to

4 said catheter body while controlling the tension on said  
5 reinforcing member while being applied thereto thus to  
6 control the depth of penetration of the reinforcement  
7 member beyond the outer surface of said catheter body  
8 toward the axis thereof, thereby to control the location  
9 of said reinforcement member in said finished catheter.

1           32. The method as set forth in claim 20  
2 wherein said catheter body is made from a thermoplastic  
3 material, and wherein the step of applying includes the  
4 step of heating said thermoplastic catheter body  
5 sufficient to permit the reinforcing member to cause the  
6 outer surface of said catheter body to become irregular  
7 when applied thereto.

1           33. The method as set forth in claim 20  
2 wherein the step of heating includes the step of heating  
3 both the thermoplastic catheter body and the reinforcing  
4 member while being applied thereto.

1           34. The method as set forth in claim 20  
2 wherein said catheter body is made from a curable  
3 material, said method including the step of curing said  
4 catheter body after the application of said reinforcing  
5 member thereto.

1           35. The method as set forth in claim 33  
2 wherein the step of curing is carried out immediately  
3 following the step of smoothing.

1           36. The method as set forth in claim 20  
2 further including the step of periodically excising a  
3 selected length of said reinforcement member from said  
4 catheter body to form a catheter having paced reinforced  
5 and non-reinforced lengths.

1           37. The method of claim 20 wherein said  
2 reinforcing member is a braid comprising a plurality of

3 reinforcing members applied to said catheter body in a  
4 spaced array.

1           38. The method as set forth in claim 20  
2 wherein said the step of applying a reinforcing member  
3 further comprises a step of applying a length of  
4 reinforcing material at a preselected helix angle to said  
5 catheter body relative to its axis.

1           39. The method as set forth in claim 38  
2 wherein the step of applying said reinforcing member at  
3 a preselected helix angle further comprising the step of  
4 rotating a guide carrying said reinforcing member in a  
5 path approximately normal to the axis of said catheter,  
6 the helix angle being defined by the length of movement  
7 of the catheter body for each rotation of said guide, and  
8 further comprising the step of ceasing rotation of said  
9 guide to decrease said helix angle relative to the axis  
10 of said catheter to define a length of catheter body in  
11 which said reinforcing member lies near the surface  
12 thereof during the time the guide has ceased rotating,  
13 whereby excising of said reinforcing member from the  
14 surface of said catheter may be carried out to excise  
15 spaced portions of said reinforcing material from said  
16 catheter structure.

1           40. A method of continuously making catheter  
2 tubing having an internal bore of accurate dimensions in  
3 a single extrusion step without applying pressure from an  
4 external source through said internal bore, comprising  
5 the steps of;

6           applying a reinforcing material to a  
7 mandrelized tube travelling at a relatively fixed linear  
8 rate and having an external diameter about equal to the  
9 desired external diameter of catheter tubing, said tube  
10 defining an external wall surface and an internal wall  
11 surface, to locate said reinforcing material within said  
12 tube at a location intermediate said external and said  
13 internal wall surfaces and deformed said inner surfaces,

14 the applying step being carried out while said tube is  
15 sufficiently heated to exhibit a viscosity at said linear  
16 rate sufficient to permit said reinforcement material to  
17 travel under tension from a location external to said  
18 exterior wall surface to said predetermined location  
19 within said tube adjacent said material, the temperature  
20 of said tube and the tension on said reinforcing material  
21 being selected to cooperate to carry out effectively said  
22 applying step for the material of said tube when  
23 traveling at said linear rate; and

24 causing said tube with said reinforcement  
25 embedded therein to cool sufficiently to solidify, thus  
26 to embed said reinforcement therein.

1 41. A continuous method of making a finished  
2 reinforced catheter from a thermoplastic material having  
3 an inner diameter and an outer diameter with a single  
4 extrusion step and without application of pressure from  
5 an external source to said inner diameter comprising the  
6 steps of;

7 continuously extruding a mandrelized catheter  
8 body as an interim structure having an outer diameter  
9 about equal to the outer diameter of said finished  
10 reinforced catheter;

11 heating said reinforcing member to a  
12 predetermined temperature;

13 continuously applying a tensioned length of a  
14 reinforcing member to an outer surface of said interim  
15 catheter body by a guide rotating in a plane  
16 approximately normal to movement of the catheter body to  
17 define a helix angle determined by the ratio of the  
18 length through which the tube advances for each complete  
19 rotation of the guide;

20 the step of applying being carried out while  
21 said catheter body is sufficiently viscous to permit  
22 deformation at a surface contour of said catheter body by  
23 an amount at least equal to the volume of said  
24 reinforcing member through a wall of said catheter body  
25 to locate said reinforcing member entirely therein at a

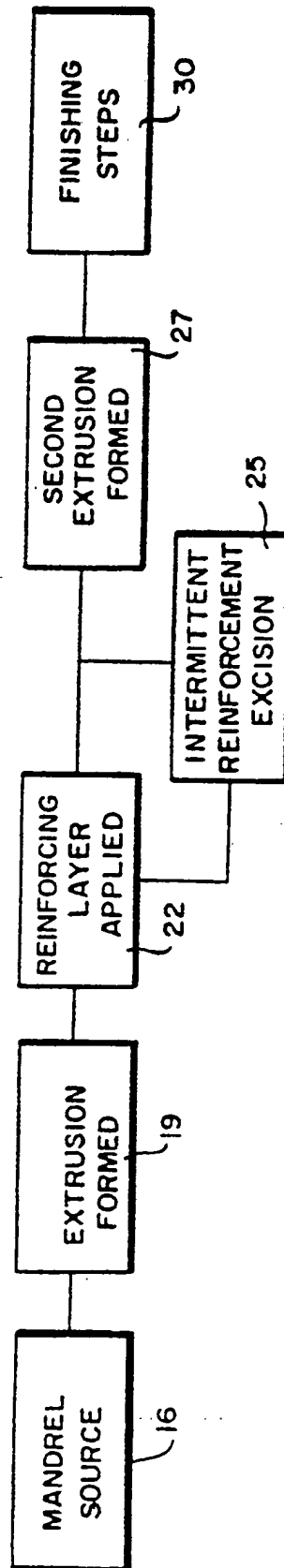


26 location determined by said viscosity and tension on said  
27 reinforcing member while the length of reinforcing member  
28 is applied thereto; and  
29           said location interrupting said inner diameter  
30 to cause said inner diameter to become irregular, thus to  
31 define at least a land having an I.D. less than the I.D.  
32 of said inner diameter.

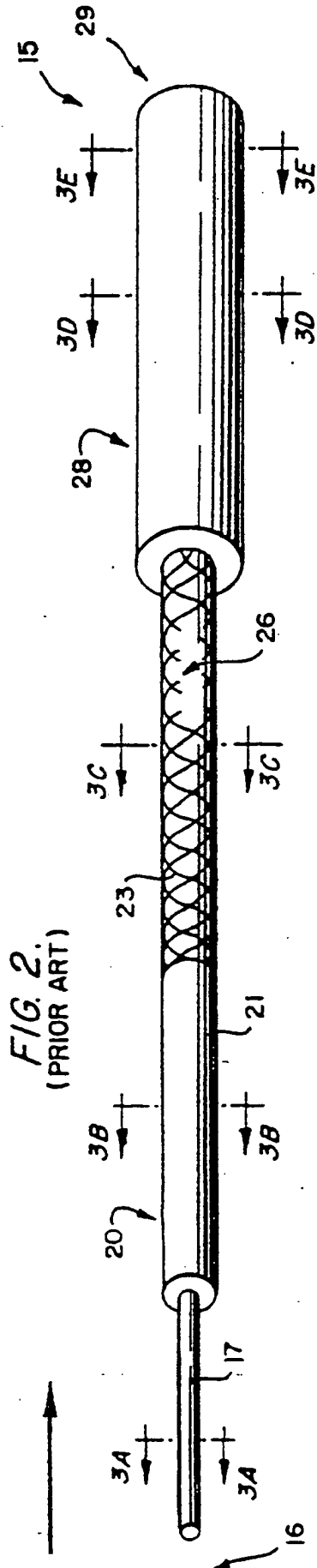
1/6

FIG. 1.  
(PRIOR ART)

15



2/6



**FIG. 3A.**  
(PRIOR ART)



**FIG. 3B.**  
(PRIOR ART)



**FIG. 3C.**  
(PRIOR ART)

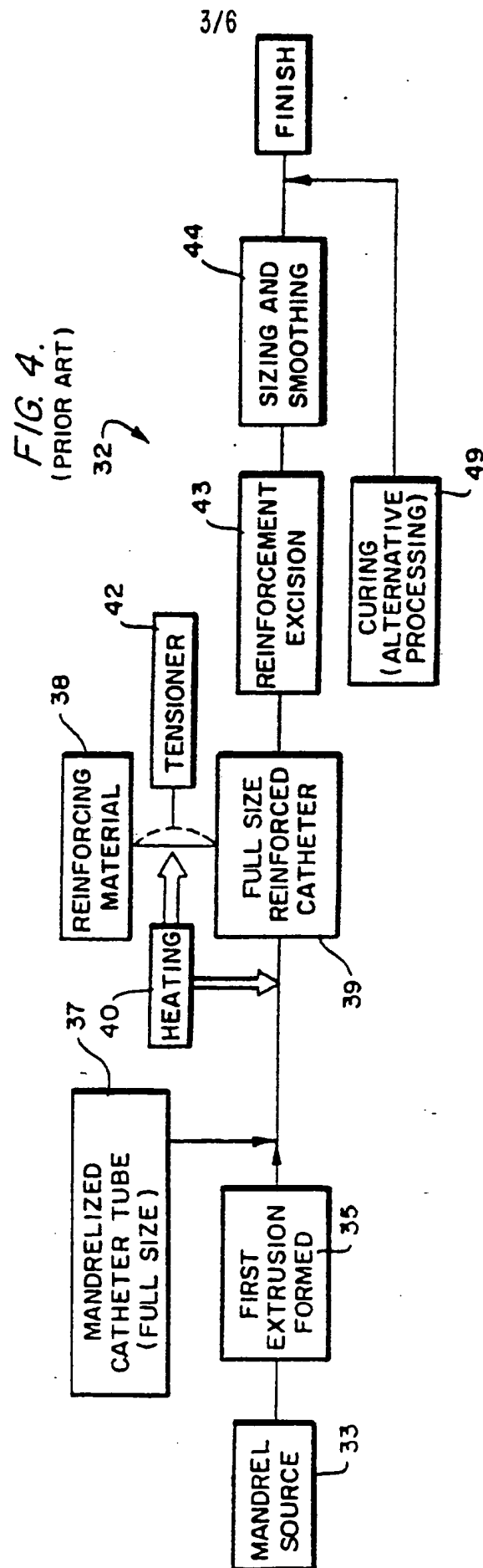


**FIG. 3D.**  
(PRIOR ART)



**FIG. 3E.**  
(PRIOR ART)





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FIG. 5.

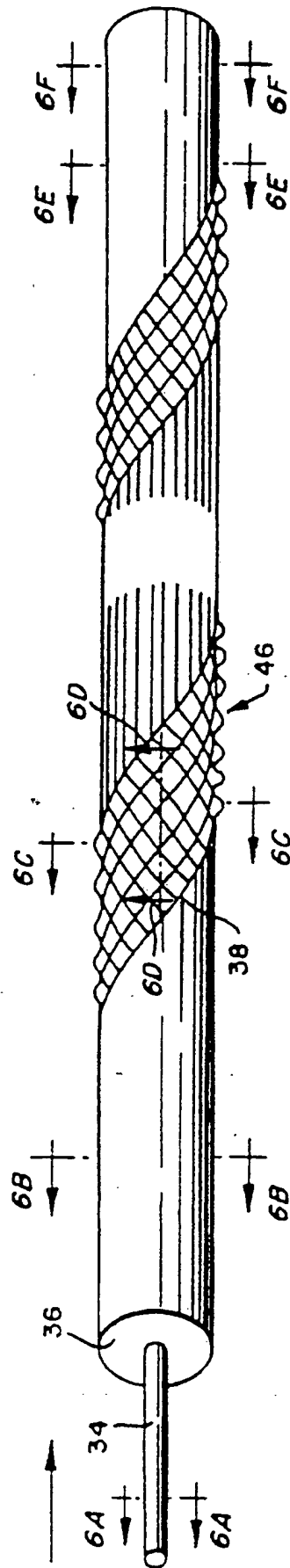


FIG. 6D.

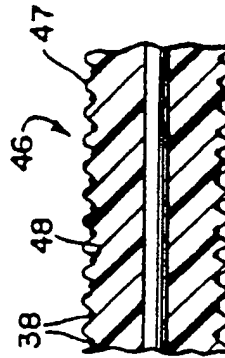


FIG. 6C.

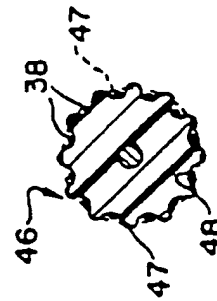


FIG. 6B.

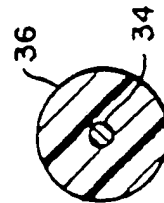


FIG. 6E.

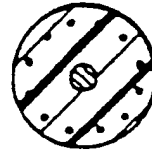


FIG. 6F.

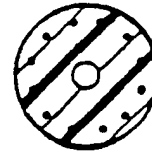


FIG. 6A.



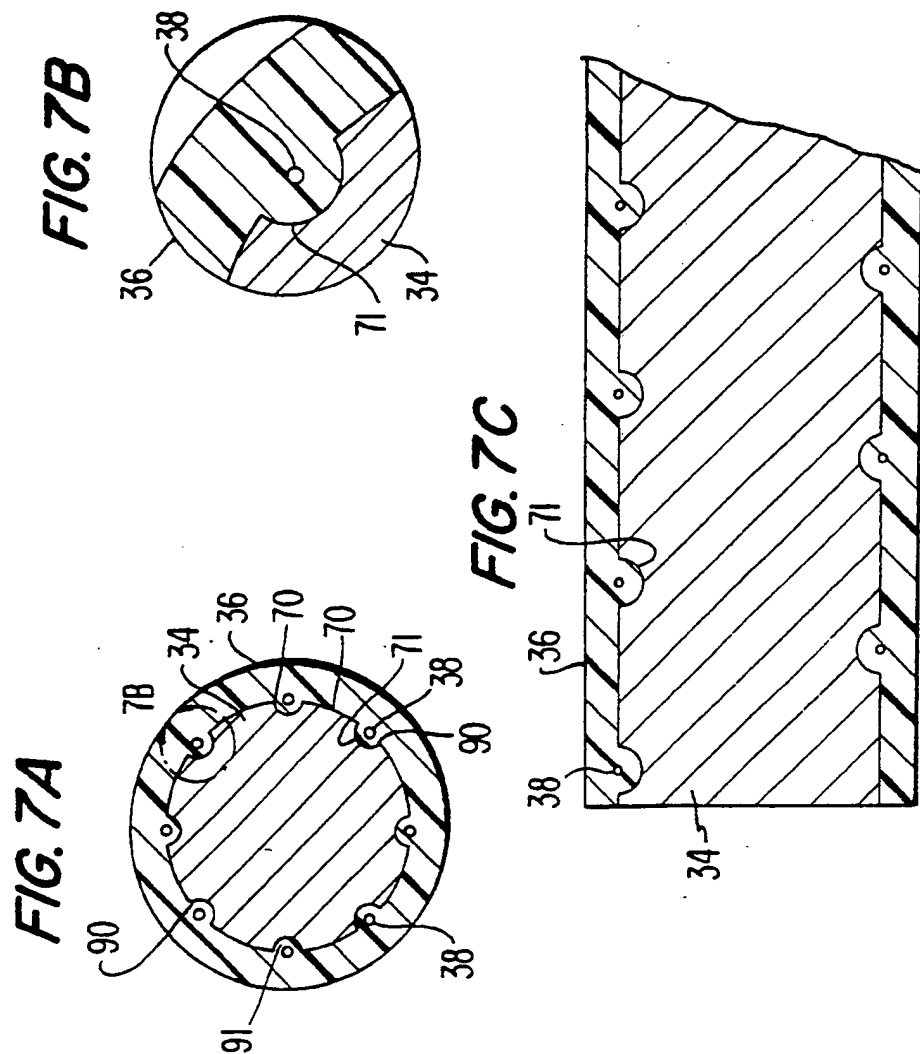


FIG. 8A

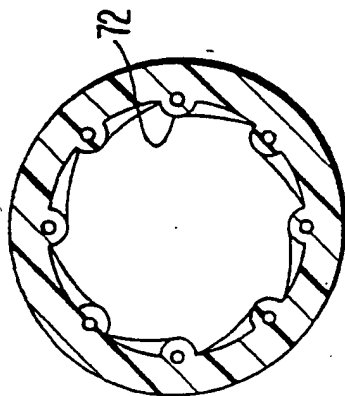


FIG. 8B

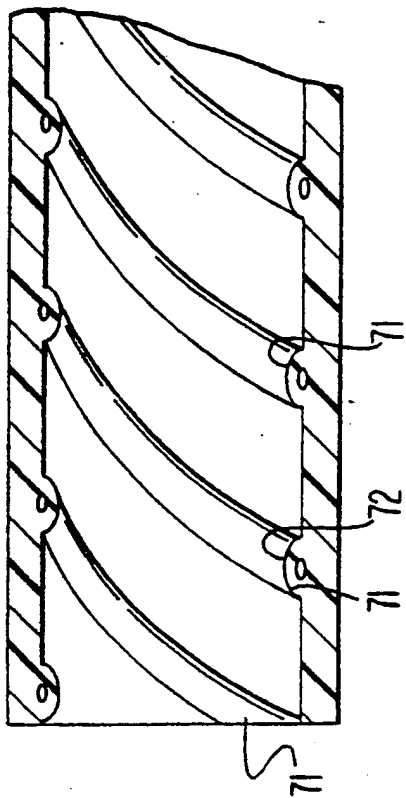


FIG. 9A

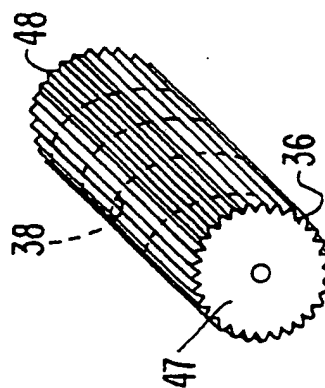
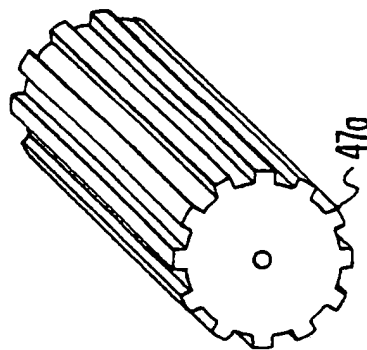


FIG. 9B



## INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US92/03668**A. CLASSIFICATION OF SUBJECT MATTER**

IPC(5) :A61M 25/01; B29C 47/02

US CL :604/282; 264/173

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 604/282; 264/173; 264/209.4, 284

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

NONE

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

NONE

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	GB, A, 2,207,902 (CRAIG MEDICAL PRODUCTS LIMITED) 15 February 1989, See the entire document.	1-8
Y	SU, A, 1,618,422 (ADAMYAN) 07 January 1991, See the entire document.	6-9
Y,E	US, A, 5,125,909 (HEIMBERGER) 30 June 1992 See the entire document.	6-9
Y	US, A, 4,832,681 (LENCK) 23 May 1989 See the entire document.	6-9
Y	US, A, 3,428,046 (REMER ET AL.) 18 February 1969 See the entire document.	1-9
Y	US, A, 4,764,324 (BURNHAM) 16 August 1988 See the entire document.	1-41
Y	US, A, 3,419,010 (WILLIAMSON) 31 December 1968 See the entire document.	1-41
A	US, A, 4,955,862 (SEPETRA) 11 September 1990	
A	US, A, 4,955,859 (ZILBER) 11 September 1990	

☒ Further documents are listed in the continuation of Box C.
 ☐ See patent family annex.

* Special categories of cited documents:	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"A" document defining the general state of the art which is not considered to be part of particular relevance	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"E" earlier document published on or after the international filing date	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"G" document member of the same patent family
"O" document referring to an oral disclosure, use, exhibition or other means	
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search 31 JULY 1992	Date of mailing of the international search report 10 SEP 1992
Name and mailing address of the ISA/ Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231 Facsimile No. NOT APPLICABLE	Authorized officer <i>James Lowe</i> JAMES LOWE Telephone No. (703) 308-3834



## INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US92/03668

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US, A, 4,950,232 (RUZICKA ET AL.) 21 August 1990	
A	US, A, 4,927,413 (HESS) 22 May 1990	
A	US, A, 4,917,666 (SOLAR ET AL.) 17 April 1990	
A	US, A, 4,705,511 (KOCÁK) 10 November 1987	
A	US, A, 3,783,454 (SAUSSE ET AL.) 08 January 1974	
A	US, A, 3,618,613 (SCHULTE) 09 November 1971	